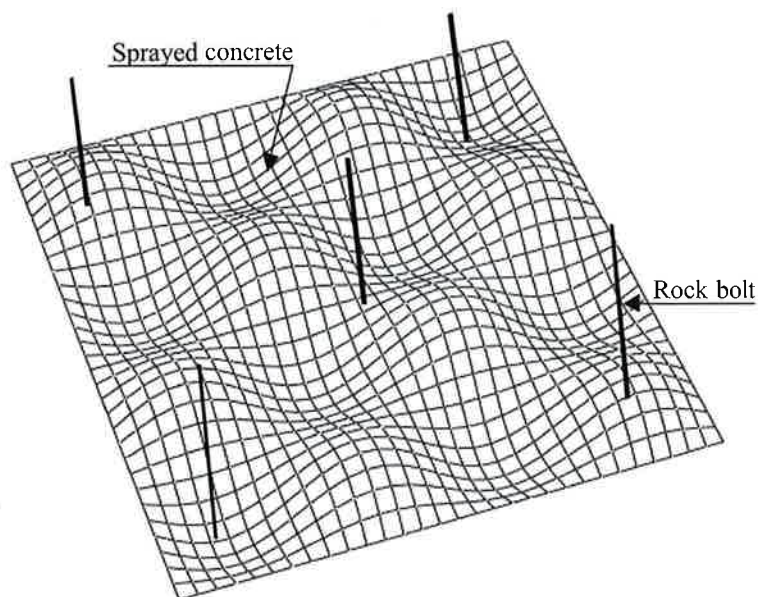


8042



ROYAL INSTITUTE OF TECHNOLOGY
STRUCTURAL ENGINEERING
SE-100 44 STOCKHOLM

Structural behaviour of fibre reinforced sprayed concrete anchored in rock

Ulf Nilsson



KUNGL TEKNISKA HÖGSKOLAN
BYGGKONSTRUKTION

TRITA-BKN. Bulletin 71, 2003
ISSN 1103-4270
ISRN KTH/BKN/B--71--SE

Doctoral Thesis

Abstract

The main objective of this investigation was to create a better foundation for design of a bolt-anchored tunnel lining. Mechanisms that influence the load bearing capacity such as compressive arch action and the irregular shape of the lining have been especially studied. A thorough investigation of the punching capacity has also been performed.

It has been shown that compressive arch action has a considerable positive effect on the load bearing capacity of fibre reinforced concrete. Punching tests were performed on circular symmetrically loaded slabs that symbolised a full-scale model of sprayed concrete around a rock bolt. A thick steel ring was placed around some of the slabs in order to incorporate the effect of compressive arch action on the failure. This ring simulates to a certain degree the restraint against lateral movements that the corresponding surrounding parts in a real lining would provide on a local failure zone. All slabs that were tested without a surrounding steel ring and could freely rotate along the support failed in bending without any signs of punching. The slabs that were tested with a lateral confinement received a considerably higher load bearing capacity and a changed failure behaviour that in many cases may be regarded as pure punching. The increase of load bearing capacity due to the surrounding steel ring was caused by compressive arch action, which also transformed the failure into punching. Increasing the fibre content from 30 kg/m^3 to 60 kg/m^3 gave no observable effect on the structural response of the slabs. A comparison between existing calculation/design methods for punching and test results showed that these methods are not fully valid for a bolt-anchored tunnel lining. Finite element simulations indicated that the failure is almost inverse to the traditional mechanism of punching.

The influence of the irregularity of the tunnel surface on the structural behaviour of the sprayed concrete was studied with numerical calculations using non-linear finite element analysis. A portion of a tunnel lining with a bolt placed at its centre showed that the stiffness is more affected by the irregularity than the load bearing capacity. If the bolts were consistently placed at the peaks or at the depressions in the lining, a completely different structural behaviour was observed. The load bearing capacity became considerably higher if the bolts were located at the peaks. This can be explained by the fact that the lining acted as compressed domes between the bolts and hence the high load bearing capacity.

Key words: *sprayed concrete, steel fibre, rock bolt, flexure, compressive arch action, non-linear finite element analysis, punching failure, irregular shape*

Contents

1. Introduction	1
1.1 Background.....	1
1.2 Sprayed tunnel linings	1
1.2.1 Design philosophy	2
1.3 Aims and scope.....	4
2. Load bearing mechanisms	6
2.1. Adhesion.....	6
2.2 Bending.....	7
2.3 Compressive arch action.....	11
2.4 Irregularities of the concrete shell	13
2.5 Punching shear.....	15
3. Studied failure mechanisms	17
3.1 Rock failures and failure mechanisms in the sprayed concrete.....	17
3.1.1 General.....	17
3.1.2 Stiff blocks.....	20
3.1.3 Cracked blocks	22
4. The effect of compressive arch action	26
4.1 Load bearing capacity according to yield line theory and compressive arch action on fibre reinforced concrete.....	26
4.1.1 Yield line theory on fibre reinforced concrete.....	26
4.1.1.1 Oblong failure zone	28
4.1.1.2 Square failure zone	29
4.1.1.3 Rectangular failure zone	30
4.1.1.4 Circular failure zone	32
4.1.2 Compressive arch action.....	34
4.1.2.1 Oblong failure zone	37
4.1.2.2 Square failure zone	44
4.1.2.3 Rectangular failure zone.....	48
4.1.2.4 Circular failure zone	52
4.2 A comparison between test results and calculated load bearing capacities according to compressive arch action.....	56
4.2.1 Beam tests.....	56

4.2.1.1 Results	58
4.2.2 Slab tests	59
4.2.2.1 Results	61
4.3 Comparison between yield line theory and compressive arch action.....	63
4.3.1 40 mm of sprayed concrete.....	63
4.3.2 80 mm of sprayed concrete.....	65
4.4 Some decreasing effects on the load bearing capacity of compressive arch action	67
4.4.1 Creep.....	67
4.4.2 Geometry	69
4.5 Conclusions	70
5. Punching shear.....	71
5.1 Introduction	71
5.2 Literature study.....	72
5.2.1 Experimental investigations	72
5.2.2 Theoretical solutions to punching shear, design codes and proposed calculation methods.....	82
5.3 Description of own tests	94
5.3.1 Introduction	94
5.3.2 Manufacturing of specimens	94
5.3.3 Material.....	95
5.3.4 Control specimens	95
5.3.5 Slab tests.....	96
5.4 Test results.....	100
5.4.1 General.....	100
5.4.2 Control specimens	100
5.4.2.1 Fibre amount 30 kg/m ³	100
5.4.2.2 Fibre amount 60 kg/m ³	102
5.4.3 Slabs.....	102
5.4.3.1 Slabs with a fibre content of 30 kg/m ³	107
5.4.3.2 Slabs with a fibre amount of 60 kg/m ³	115
5.5 Comparison of observed punching capacities with predictions	118
5.6 Stiffness of the lateral confinement caused by steel ring and by the assumed wedge in the lining	121
5.7 Conclusions	122
6. Numerical analyses of the punching failure	124
6.1 Introduction	124

6.2	Analysis tool	124
6.3	Material model.....	124
6.4	The finite element model and loading	128
6.5	Results	130
6.5.1	Slabs loaded with a stiff cylinder	130
6.5.1.1	Load-deflection response.....	130
6.5.1.2	Cracks	132
6.5.1.3	Strains	135
6.5.2	Slabs loaded with a slender plate.....	139
6.5.2.1	Load-deflection response.....	139
6.5.2.2	Cracks	141
6.5.2.1	Strains	143
6.5.3	Slabs with different degrees of lateral confinement	147
6.5.3.1	Load-deflection response.....	147
6.5.3.2	Tangential cracks and principal strains at maximum load	149
6.6	Conclusions	151
7.	The irregular shape of the lining.....	153
7.1	Introduction	153
7.2	Analysing tool.....	154
7.3	Material model.....	154
7.4	The finite element model and loading	156
7.5	Results	158
7.5.1	Slab with a bolt placed at its centre located at an peak or at a depression	158
7.5.1.1	Relative stiffness.....	158
7.5.1.2	Relative load bearing capacity.....	159
7.5.1.3	Principal stresses.....	162
7.5.2	Slab with bolts consistently placed at the peaks or at the depressions	169
7.5.2.1	Load-deflection response.....	169
7.5.2.2	Principal stresses.....	170
7.6	Conclusions	175
8.	General conclusions and needs for further research.....	176
8.1	General conclusions.....	176
8.2	Needs for further research	178
9.	References.....	179

Appendix	184
A Calculation scheme of compressive arch action for different failure zones	
B Node generation of an irregular shell using mathcad as a pre-processor	
C ABAQUS-code of an irregular concrete slab with a support at its centre	
D ABAQUS-code of a reference beam	